Investigation of Internal Plasma Structure in an Anode-layer Hall Thruster

IEPC-2007-092

Presented at the 30th International Electric Propulsion Conference, Florence, Italy September 17-20, 2007

Nanako Takahashi*, Naoji Yamamoto†, Hideki Nakashima‡

Department of Advanced Energy Engineering Science, Kyushu University, 6-1 Kasuga-kouen, Kasuga, Fukuoka 816-8580, Japan

Shigeru Yokota[§], Kimiya Komurasaki** and Yoshihiro Arakawa^{††}

Department of Aeronautics and Astronautics The University of Tokyo, Hongo 7-3-1, Bunkyo-ku, Tokyo, 113-8656, Japan

Abstract: Internal plasma structure in a Hall thruster was measured with the objective of understanding physics in Hall thrusters. The plasma parameter, plasma potential, electron temperature and number density were measured by means of electrostatic probe using a 1 kW class anode layer type Hall thruster. The anode layer was observed under low magnetic field condition, and the position that the potential is falling, goes upstream, toward anode, with increase in magnetic flux density. The measurement electron temperature and number density in the acceleration channel are 20 eV and $3x10^{18}$ m-3, respectively. The ionization zone also goes upstream with increase in magnetic flux density. Electron diffusion coefficient was estimated using above results. These results showed that the transition in operational regime at critical magnetic flux density is caused by the transition in electron diffusion from classical to anomalous diffusion.

Nomenclature

B: magnetic flux densityD: diffusion coefficientE: electric field strength

d: distance between two probes

e: electronic charge

I : current

L: ionization zone length

m: particle mass \dot{m} : mass flow rate N: number density S: cross-section

* Research student, Department of Advanced Energy Engineering Science, nanako@aees.kyushu-u.ac.jp.

[†] Assistant Professor, Department of Advanced Energy Engineering Science, <u>vamamoto@aees.kyushu-u.ac.jp.</u>

[‡] Professor, Department of Advanced Energy Engineering Science,nakasima@aees.kyushu-u.ac.jp

[§] Doctor candidate, Department of Aeronautics and Astronautics , yokota@al.t.u-tokyo.ac.jp

^{**} Associate professor, Department of Aeronautics and Astronautics , komurasaki@al.t.u-tokyo.ac.jp

^{††} Professor, Department of Aeronautics and Astronautics ,arakawa@al.t.u-tokyo.ac.jp

T: temperature $V_{\rm d}$: discharge voltage z: axial direction Δ : oscillation amplitude

 μ : mobility

 σ_{di} : atom ionization collision cross-section

 $\sigma_{\scriptscriptstyle T}$: atom total collision cross-section

 τ : measurement time = 5 ms

 ϕ : diameter

Subscripts

B : Bohm diffusion c : classical diffusion

e : electron

eff: effective coefficient

d : dischargei : ion

n : neutral atom
r : radial direction
0 : anode side
1 : exit side

I. Introduction

Hall thruster is a promising thruster for satellite station keeping and orbit transfer applications¹⁻³ because it has a high thrust efficiency exceeding 50% with a specific impulse range of 1000–3000 s, delivering higher thrust-to-power ratio as compared to ion thrusters. Therefore, there were and will be many missions using a Hall thruster⁴, e.g., SMART-1 lunar mission⁵, MBSAT, and Lockheed-Martin Space Systems GEO satellites⁶.

One of the challenges presented by Hall thrusters is the discharge current oscillation, particularly at a frequency range of 10–100 kHz. The Due to the reduction in the impact of the Power Processing Unit (PPU) and the enlargement of the surplus for the power supply of the satellite system, it is preferable to maintain a low level of discharge current oscillations. The oscillation may also affect the erosion of the acceleration channel or the ion beam divergence. Understanding the oscillation is essential for the future improvement of Hall thrusters, particularly of the anode layer type. Several studies have been conducted on this oscillation phenomenon, and they have revealed that the oscillation is caused by ionization instability. However, these studies did not adequately describe the oscillation, and in particular, do not determine the stability criteria for a given range of magnetic flux density. Measuring internal plasma structure in Hall thrusters is essential for describing this oscillation mechanism. It also helps the understanding the ionization and electron diffusion mechanism in the Hall thruster. Furthermore, this information will play an important role in the validation of numerical models. There have been many studies about measuring internal structure in a magnetic layer type Hall thruster. 15-17 On the other hand, there are few studies about that in an anode layer type. Comparison between the two types would give invaluable knowledge of ionization and electron diffusion mechanisms in Hall thrusters.

Therefore, the aim of this study is measuring internal plasma structure in the anode layer type Hall thruster and understanding these mechanisms in Hall thrusters.

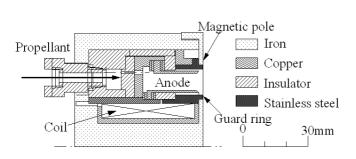
II. Experimental Equipment

A. Anode Layer Type Hall Thruster

Figure 1 shows the cross-section of a 1 kW class, anode layer type Hall thruster. 18-22 The inner and outer diameters of the acceleration channel are 48 mm and 72 mm, respectively. A solenoidal coil is set at the center of the thruster to apply a radial magnetic field in the acceleration channel. The magnetic flux density is varied by changing the coil current. There is no outer coil because a uniform magnetic field distribution is maintained along the

azimuthal direction. The magnetic field distribution along the channel median is almost uniform in the short acceleration channel, as shown in Fig.2. Magnetic flux density is maximized in the inner wall and decreases with a decrease in radius since the magnetic flux is constant. Thus, in this study, the magnetic flux density at the channel median is assumed to be representative. The guard rings are made of stainless steel (SUS304). The separation between the guard ring and the anode is 1 mm. It has a hollow annular anode, which comprises two cylindrical rings, and a propellant gas is fed through them. The position and the width of the hollow anode are varied by changing the anode components. In this study, the width of the hollow anode is 8 mm, and the gap between the tip of the anode and the exit of the acceleration channel is fixed at 3 mm.

High-purity (99.999% pure) xenon gas was used as the propellant. Thermal mass flow controllers (Kofloc, 3610) are used. A hollow cathode (Veeco-Ion Tech, HC-252) was used as the electron source.



Anode Exit

Anode

Order of the state of the

Figure 1. Cross section of the anode layer type Hall thruster developed at the University of Tokyo.

Figure 2. Magnetic field profile along z axis.

B. Electrostatic Probe

For the measurement of plasma density and electron temperature in the acceleration channel, double Langmuir probe was used. The schematic of this probe was shown in Fig. 3. The double probe consisted of two 0.15 mm in diameter and 1.8 mm in length cylindrical tungusten wire electrodes insulated from each other by two alumina insulators. The diameter of the prove, r_p and the distance between the two electrodes, d are chosen based on the standard probe theory as below.

1. The distance between two is larger than the twice of Debye length in order to avoid electrode interaction.

$$d > 2\lambda_D = 2 \times \sqrt{\frac{\varepsilon_0 k T_e}{e^2 n_e}} \approx 10^{-4} \quad \text{m}$$
 (1)

2. Collisionless plasma

$$r_p \ll \lambda_e, \quad \lambda_D \ll \lambda_e$$

$$\lambda_{en} = \frac{1}{n_n \sigma} \approx \frac{1}{10^{20} \times 10^{-19}} \approx 10^{-1} \text{m}$$

$$\lambda_{ee} \approx \lambda_{ii} \approx \lambda_{ei} = \frac{1}{n_p \sigma} = \frac{16\pi \varepsilon_0^2 m^2 v^4}{e^4 n_p} \approx 10^{-1} \text{ m}$$
(2)

3. Conventional thin sheath

$$\lambda_D < r_p \tag{3}$$

In order to minimize probe heating as much as possible in the acceleration channel, high speed linear motor reciprocating positioning system was used. This system lets the staying period in the acceleration channel be 52 ms when the most upstream position of the probe is 5.1mm upstream of the exit, as shown in Fig.4. In this study, plasma property in the channel median was measured. Applied voltage between two electrodes is swept as Sine function (the amplitude =100 V, the frequency = 400 Hz). Though the probe was moved 0.3 mm within sweeping period, this influence on the measurement is little, since 0.3 mm is less than 1.8 mm, the probe length. The error is about 20 %, which derived from the standard

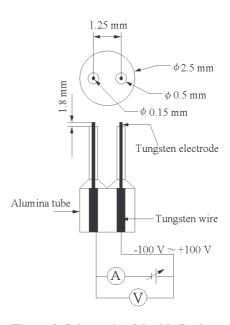
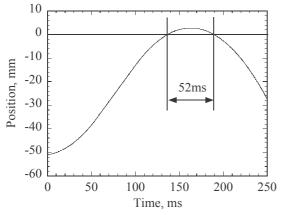


Figure 3. Schematic of double Probe.

deviation of measurement, the fitting error, and the probe processing accuracy.

The emissive probe was made of a 0.1mm in diameter 0.1% thoriated tungsten as shown in Fig. 5. A linear motor was used to insert the emissive probe into the discharge chamber. It provides linear reciprocating motion at very high motion and acceleration.



 ϕ 0.1 Thoriated Tungsten wire ϕ 0.5 mm Tungsten wire

Figure 4. Probe position trace.

Figure 5. Schematic of emissive probe.

C. Vacuum Chamber

A vacuum chamber of 2 m diameter by 3 m length was used in the experiments. The pumping system comprised a diffusion pump, a mechanical booster pump, and two rotary pumps. The background pressure was maintained below 5.3×10^{-3} Pa for most of the operating conditions.

D. High-speed Camera

An image intensified high-speed camera (DRS Technologies Inc., Product, ULTRA 8) was used for the observation of the plasma. The maximum frame rate of this camera is 100,000,000 fps.

E. Ion Collector

An ion beam current was measured using the ion beam collector (500 mm \times 500 mm nude plane collector) that was located at 250 mm downstream of the thruster. Compensation for the decay of the ion beam current by charge-exchange was performed according to the method described in Ref. 23. The charge-exchange cross section was obtained from Ref. 24. The friction of the double xenon ion was assumed to be 0.2. ^{25, 26} The total error of this compensation did not exceed 5%, and the largest source of error is the ionization gauge.

III. Results and Discussion

The discharge current and the amplitude of the discharge current oscillation should be a good indicator of operational condition. In order to evaluate the oscillation depth in the experimental results, the amplitude of oscillation, Δ is defined as,

$$\Delta = \frac{R.M.S}{\overline{I_d}} = \frac{1}{\overline{I_d}} \sqrt{\frac{\int (I_d - \overline{I_d})^2}{\tau}}, \quad (\overline{I_d} = \frac{\int I_d}{\tau})$$
 (4)

Figure 6 shows the relation between the discharge current and the amplitude of 10 kHz range oscillation against magnetic flux density. The discharge current is decreased with increase in B in B < 23 mT, and then it is increased with B. The oscillation amplitude is also decrease in B. Stable operation was observed in a

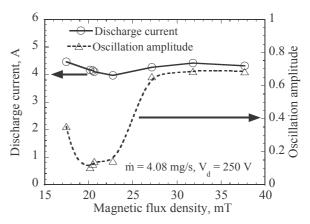


Figure 6. Operation characteristics.

narrow range near B \approx 20 mT in this configuration. The oscillation amplitude suddenly increases at B= 24 mT. Thus, the operational condition range is narrow, and hence an extension of the stable operational condition range is required. This sensitivity to B indicates that the oscillation would be dominated by electron mobility rather than by ion mobility.

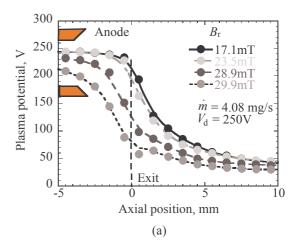
Figure 7(a), (b), and (c) show the plasma potential distribution, electron temperature distribution, and number density distribution along the axis. respectively. So-called "anode layer" was observed under low magnetic field condition. In this thin laver. ionization and acceleration would be occurred. The position that plasma potential is falling goes upstream, toward the anode, with increase in magnetic flux density. This would lead the ionization zone to go upstream with increase in magnetic flux density, as shown in Fig.5(c). On the other hand, when B > 27 mT, where the oscillation amplitude is large, the potential is falling inside the hollow anode and cannot observed anode layer. In Hall thrusters, the Lorentz force, derived from the interaction between the Hall current and magnetic field, prevents electrons from going upstream and keeps the strong electric field in the acceleration channel. Therefore, with increase in the coil current, the magnetic field inside the hollow anode is also increased and then electric field strength inside of the hollow anode is also increased. Therefore, the plasma potential is falling inside the hollow anode.

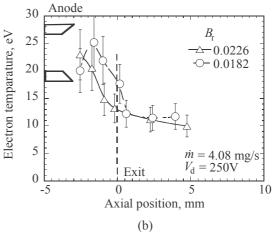
The electron temperature and number density in the ionization zone are 23 eV and 3.3×10^{18} m⁻³, respectively, which are higher than those of magnetic layer type. ¹⁹ This high electron temperature is due to the low electron energy losses to the acceleration channel wall. There is little interaction between the wall and the electrons, since the anode layer type has a conducting wall which potential are kept in a cathode potential.

With the potential profile changing, the electron temperature profile and the electron number density profile are changed; the electron temperature has a positive correlation with downstream electric field strength, therefore, the zone, where electron temperature is high, goes upstream with the increase in magnetic coil current. The ionization zone, which exists where the potential is falling, also goes upstream with high temperature zone going upstream.

The 0D-oscillation model shows that the conditions of stable operations is written as follows:¹⁴

$$S_1 V_{e_1} - S_0 V_{e_0} - \overline{\langle \sigma_{di} v_e \rangle}_{T_e} \overline{N}_n SL > 0$$
 (5)





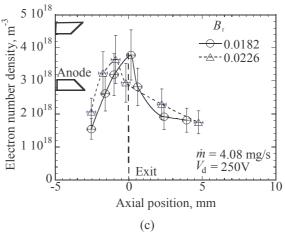


Figure 7. Plasma parameter profile.

- (a) Axial profile of plasma potential.
- (b) Axial profile of Electron temperature.
- (c) Axial profile of Electron number density. $\dot{m} = 4.08 \text{ mg/s}, V_d = 250 \text{ V}$

Table.1 Typical measurement values for estimation of diffusion coefficient.

Parameter	Classical diffusion regime	Anomalous diffusion regime
$\eta_{ m E}$	0.9	0.8
$T_{\rm e}$, eV	16	12
E, V/m	60,000	24,000

The left hand side of Eq. (5) represents the momentum transfer corresponding to fluctuations of plasma, i.e., viscosity effects. Thus, the oscillations decay if the viscosity coefficient, i.e., the left hand side of Eq. (5), is positive.

According to the Eq.(5), the increase in plasma density in the vicinity of the anode would have operation unstable, therefore, with increase in magnetic flux density would cause the operation to be unstable.

Electron diffusion mechanism is one of the most significant mechanisms for Hall thruster, so we estimate the diffusion coefficient at the acceleration channel exit. The diffusion coefficient at the acceleration channel exit is estimated by as follows:

$$D = \frac{\Gamma_{\rm e}}{S N_{\rm e} (\frac{e}{kT_{\rm e}} E + \frac{\nabla n_{\rm e}}{N_{\rm e}})} \Rightarrow D_{\rm 1} \approx \frac{I_{\rm d} - I_{\rm i}}{e S_{\rm 1} N_{\rm il} \frac{e}{kT_{\rm el}} E_{\rm 1}} \tag{6}$$

 $I_{\rm i}$ was measured by the ion collector and the number density of ions was estimated as follows:

fions was estimated as follows:

$$N_{i1} = \frac{I_i}{eS_1 V_{i1}} \approx \frac{I_i}{eS_1 \sqrt{\frac{2\eta_E eV_d}{M}}}$$
(7)

The values of beam energy efficiency, 17 E, and $T_{\rm e}$ were assumed to be typical measurement values, as shown in Table. 1. $\eta_{\rm E}$ was measured by means of a retarding potential analyzer, 27 E was estimated to be 1.2 (300 V/250 V) times that of the above results. $I_{\rm i}$ was measured by means of the ion collector.

Figure 8 shows the estimated diffusion coefficient at the acceleration channel exit. The diffusion coefficient decreases with increase in B and suddenly increases at $B=27\,$ mT, and then decreases with B, again. The transition at $B=27\,$ mT is caused by the transition in electron diffusion from classical to anomalous diffusion. That is, an electron moves toward the anode via classical diffusion when $B<27\,$ mT, and it moves via anomalous diffusion when $B>27\,$ mT, as shown in Fig. 8. There is some transition regime at $15\,$ mT $< B < 27\,$ mT. It is noteworthy that the oscillation regime also changes at this point. This was another indication that the oscillation is sensitive to electron mobility.

Several MHz oscillations can be observed when B > 27 mT. This oscillation cannot be observed when B < 27 mT. This result shows these MHz fluctuations in the plasma would cause this anomalous diffusion. that is,

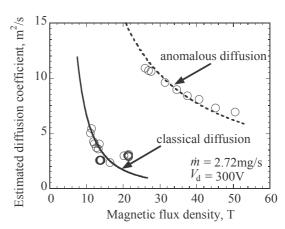
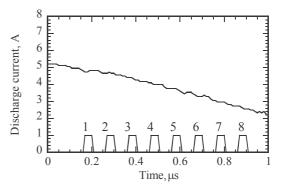


Figure 8 Estimated electron diffusion coefficient.



Frame rate: 10000000 fps Exposure time: 50 ns

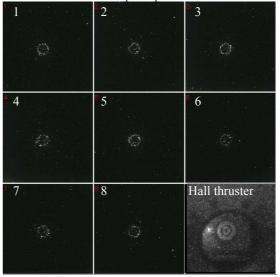


Figure 9. Plasma behavior. $\dot{m} = 2.72 \text{ mg/s}, V_d = 300 \text{ V} B = 0.046 \text{ T}$

with infinite small perturbation, the mobility is described as follows,

$$\mu_e = \frac{m_e}{eB^2} \left(n_n \langle \sigma v \rangle_{en} + \frac{\pi}{4} \frac{eB}{m_e} \left(\left(\frac{\Delta n_e}{n_e} \right)^2 \right) \right)$$
 (8)

Hirakawa et al. shows that the azimuthal plasma fluctuation lead to anomalous diffusion by numerical simulation.²⁸ That is, the interaction between azimuthal electric field fluctuations and radial magnetic field cause the charged particles to be drift in the z axial direction and the order of this is almost the same as that of the Bohm diffusion.

In order to investigate these MHz oscillations, the plasma behavior was observed by means of a high-speed camera. Figure 9 shows the plasma behavior and the discharge current trace under the unstable condition at a frame rate of 10,000,000 fps and an exposure time of 50 ns. These pictures are not distinct pictures, but it is impossible to increase the frame rate or to decrease the exposure time, since the emission of light from the plasma is weak. However, the emission in the annular acceleration channel is not uniform in the azimuthal direction and it fluctuates with the frequency of about two MHz. This azimuthal plasma fluctuation would cause anomalous diffusion in this regime.

This fluctuation would be ion plasma instability or drift instability. But this would be derived from the drift instability, since ion plasma instability would not be affect by the magnetic field strength. Azimuthal nonuniformity in the channel would be enlarged with increase in magnetic flux density, since the ionization zone in the acceleration channel expands toward anode with increase in magnetic flux density.

IV. Conclusion

Internal plasma structure in the anode layer type Hall thruster was measured by means of electrostatic probe for understanding the mechanism in Hall thrusters.

From the results of emissive probe, so-called "Anode layer" can be observed in the low magnetic flux density, and the position where potential is falling moves toward anode with increase in magnetic coil current. With this change, the ionization zone also moves toward anode with increase in B. The electron temperature and number density in the acceleration channel is 20 eV, and $3 \times 10^{18} \text{ m}^{-3}$. It is confirmed that the electron temperature and electron number density in anode layer type Hall thruster is higher than that of magnetic layer, which suits the design concept of the anode layer Hall thruster.

The operational regime in the anode layer Hall thruster changes at critical magnetic flux density= $27 \,\mathrm{mT}$ at $\dot{m} = 2.72 \,\mathrm{mg/s}$, $V_{\rm d} = 300 \,\mathrm{V}$. This is because an electron moves toward the anode via classical diffusion when $B < 27 \,\mathrm{mT}$, and it moves via anomalous diffusion when $B > 27 \,\mathrm{mT}$. An azimuthal plasma fluctuation would cause this anomalous diffusion. That is, azimuthal electric field fluctuations caused by the azimuthal plasma fluctuation and radial magnetic field make charged particles drift in the z axial direction. The observation of plasma behavior by high-speed camera supports this assumption. This result implies that anomalous diffusion is caused not only by nearwall conductivity but also by the azimuthal plasma fluctuation in the magnetic layer type Hall thrusters. Therefore, more precious study about this several MHz Oscillations would be need for understanding the anomalous diffusion.

Acknowledgments

The present work was supported by a Grant-in-Aid for Scientific Research (S), No. 16106012, sponsored by the Japan Society for the Promotion of Science, Japan.

References

¹Gulczinksi, F. S., and Spores, R. A., "Analysis of Hall-Effect Thrusters and Ion Engines for Orbit Transfer Missions," AIAA-96-2973, 32nd Joint Propulsion Conference, July 1996.

²Kim, V., "Main physical features and processes determining the performance of stationary plasma thrusters," Journal of Propulsion and Power, Vol. 14, No. 5, pp. 736–743, 1998,

³Kaufman, H. R., "Technology of Closed-Drift Thrusters," *AIAA Journal*, Vol. 23, No. 1, 1985, pp. 78–86.

⁴Sackheim, R. L., "Overview of United States Space Propulsion Technology and Associated Space Transportation Systems," Journal of Propulsion and Power, Vol. 22, No.6, pp1310-1332. 2006.

⁵Milligan, D., Gestal, D., Camino, O., Estublier, E D., Noordwijk, Koppel, C., "SMART1 Electric Propulsion Operations,"AIAA-paper 2004-3436, Fort Lauderdale, Florida, July 11-14, 2004

- ⁶ Hofer, R.R., Randolph, T.M., Oh, D.Y., Snyder, J.S., and degrees, K.H., "Evaluation of a 4.5 kW commercial Hall thruster system for NASA science missions," AIAA-2006-4469, 42nd Joint Propulsion Conference, Sacramento, CA, Jul 2006.
- ⁷Tilinin, G. N., "High-Frequency Plasma Waves in a Hall Accelerator with an Extended Acceleration Zone," *Soviet Physics-Technical Physics*, Vol. 22, No.8, 1977, pp. 974–978.
- ⁸Choueiri, E. Y., "Plasma Oscillations in Hall Thrusters," *Physics of Plasmas*, Vol. 8, No. 4, 2001, pp. 1411–1426.
- ⁹Baranov, V. I., Nazarenko, Yu. S., Petrosov, V. A., Vasin, A. I., and Yashonov, Yu. M., "Theory of oscillations and conductivity for Hall thruster," AIAA Paper 96-3192, July 1996.
- ¹⁰Baranov, V. I., Nazarenko, Yu. S., Petrosov, V. A., Vasin, A. I., and Yashonov, Yu. M., "The Ionization Oscillations Mechanism in ACD," Proceedings of the 24th International Electric Propulsion Conference, IEPC Paper 95-059, Sept. 1995.
- ¹¹Fife, J. M., Martinez-Sanchez, M., and Szabo, J., "A numerical study of low-frequency discharge oscillations in Hall thrusters," AIAA Paper 97-3052, July 1997.
- ¹²Boeuf, J.P., and Garrigues, L., "Low Frequency Oscillation in a Stationary Plasma Thruster," Journal of Applied Physics, Vol. 84, No. 7, 1998, pp. 3541–3554.
- ¹³Komurasaki, K., and Kusamoto, D., "Optical Measurement of Plasma Oscillations in a Hall Thruster," *Transactions of the Japan Society for Aeronautical and Space Sciences*, Vol. 42, No. 134, 1999, pp. 203–208.
- ¹⁴Yamamoto, N., Komurasaki, K., and Arakawa, Y., "Discharge Current Oscillation in Hall Thrusters," of Propulsion and Power, Vol. 21, No. 5, pp. 870–876, 2005.
- ¹⁵Hass, J. M., Gallimore, A. D., McFall, K., and Spanjers, G., "development of a high-speed, reciprocating electrostatic probe system for Hall thruster interrogation," Review of science instruments, vol.71, 11,pp.4131-4138.
- ¹⁶Hargus, W.A. Jr., Cappelli, M.A., "Laser-induced fluorescence measurements of velocity within a Hall discharge," Appl. Phys. B 72, pp.961–969, 2001.
- ¹⁷Komurasaki, K., and Arakawa, Y., "Hall current ion-thruster performance," Journal of Propulsion and Power, Vol.8, No.6, pp.1212-1216, 1992.
- ¹⁸Semenkin, A., "Investigation of Erosion in Anode Layer Thrusters and Elaboration High Life Design Scheme," *Proceedings of the 23rd International Electric Propulsion Conference*, IEPC Paper 93-231, Electric Rocket Propulsion Society, Sept. 1993.
- ¹⁹Choueiri, E. Y., "Fundamental difference between the two Hall Thruster Variants," *Physics of Plasmas*, Vol. 8, No. 11, 2001, pp. 5025–5033.
- ²⁰Zharinov, A. V., and Popov, Yu. S., "Acceleration of Plasma by a Closed Hall Current," *Soviet Physics-Technical Physics*, Vol. 12, No.2, 1967, pp. 208–211.
- ²¹Popov, Yu. S., and Zolotaikin, Yu M., "Effect of Anomalous Conductivity on the Structure of the Anode Sheath in a Hall Current Ion Source," *Soviet Journal of Plasma Physics*, Vol. 3, No.2, March-April 1977, pp. 210–213
- ²²Zhurin, V. V., Kaufman, H. R., and Robinson, R. S., "Physics of Closed Drift Thrusters," *Plasma Sources Science & Technology*, Vol. 8, No.1, 1999, R1–R20.
- ²³Rapped, D., and Francis W. E., "Charge Exchange Between Gaseous Ions and Atoms," *Journal of Chemical Physics*, Vol. 37, No.11, 1962, pp.2631-2645.
 - ²⁴Sanborn, C. B., "Basic data of plasma physics, 1966," Second Edition, Rev., The MIT Press, 1967, p75.
- ²⁵Gallimore, A. D., "Near- and Far-Field Characterization of Stationary Plasma Thruster Plumes," *Journal of Spacecraft and Rockets*, Vol. 38, No. 3, 2001, pp. 441–453.
- ²⁶Manzalla, D. H., and Sankovic, J. M., "Hall Thruster Ion beam Characterization," AIAA Paper 95-2927, July
- ²⁷Kakimoto, H, "Plasma Characteristics in Anode Layer Thrusters," Masters Thesis, The Univ. of Tokyo, Department of Aeronautics and Astronautics, Mar. 2000 (in Japanese).
- ²⁸Hirakawa, M., Arakawa, Y., "Numerical simulation of plasma particle behavior in a Hall thruster," AIAA-Paper 1996-3195, Lake Buena Vista, FL, July 1-3, 1996.